



# DC/DC Conversion (bPOL, 11V $\rightarrow$ 1.5V)

Samantha Kelly

(under direction of Timon Heim, Karol Krizka, and Zhicai Zhang)

July 8th, 2022

## The Goal

- bPOL is a single-phase synchronous buck converter designed for HEP experiments (variable voltage → constant lower voltage and variable current) that is controlled by AMAC chip
  - Replacement for FEAST2 line
  - Max input voltage recommended is 11V (can technically handle 12V)
  - Max output current recommended is 4A
  - Converts variable DC voltage into constant lower DC voltage with variable current
    - Operates by applying pulse width modulated (PWM) waveform of duty cycle to low pass LC filter
      - Switch is connected to input voltage and inductor
  - Downside of buck converter: noisy
    - Nature of switching regulators

#### The Goal (cont.)

- Want to describe efficiency of DC/DC conversion performed by bPOL from 11V to 1.5V in terms of temperature (from Proportional To Absolute Temperature sensor) and output current
  - Want efficiency fit to be true for detector temperature range (-40°C to 40°C)

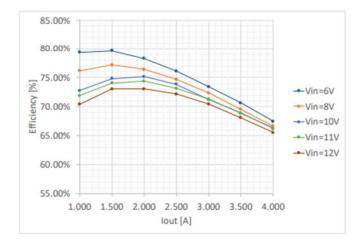
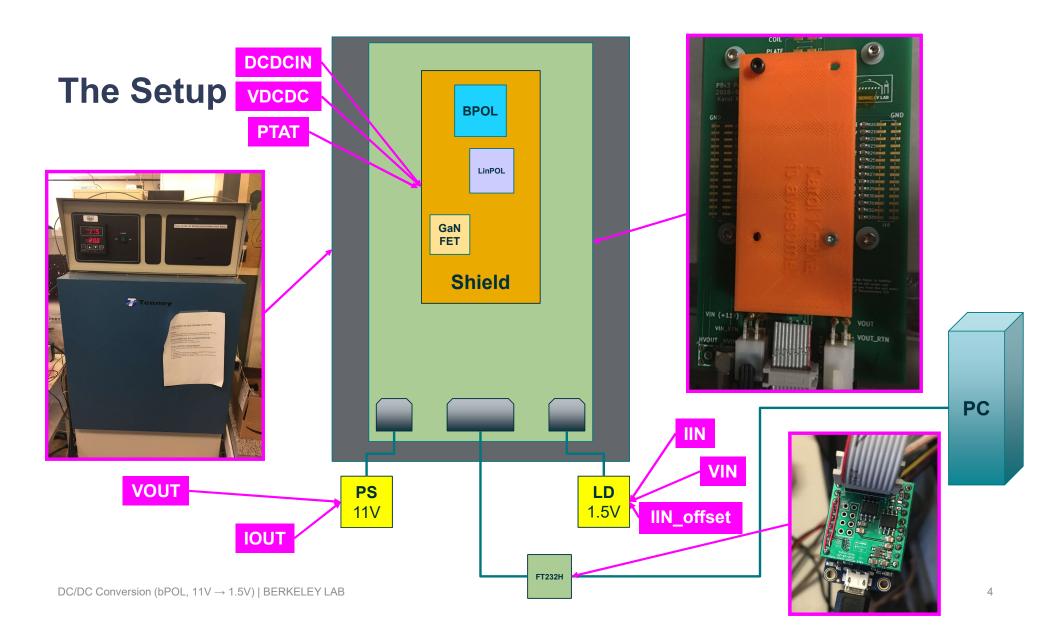


Figure 27: ASIC Efficiency for the Vout=1.5V version (without input+output  $\pi$  filters) and different Vin and Iout with the module in good thermal contact with a cooling plate at about 20°C.



# Wrangling the chiller

Takes much longer than one would think

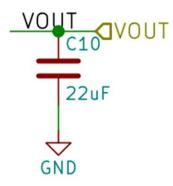
- Settings on chiller in strips lab are the same as chiller in pixel lab, but are not capable of sustaining the same temperature range
  - -30°C to -40°C impossible, 30°C to 40°C difficult
    - This means the range of temperature tests is truncated to -15°C to 35°C
- Two primary differences: cable hole stopper, and chiller maintenance
  - Cable hole stopper in pixel lab is rubber stopper, cable hole stopper in strips lab are pieces of foam
    - Sometimes foam pieces are pushed out by compressed air
    - Makes a difference, but doesn't fully account for malfunction
  - Chiller maintenance is done on individual chillers, not both uniformly, and tests generally only use one of the two chillers
    - Service being planned to ensure circulation is where it should be, etc.

## Taking data well

- Take temperature data based on PTAT reading rather than set temperature on chamber
  - For bin X, all data points corresponding to PTAT readings of  $X 2.5^{\circ}C$  to  $X + 2.5^{\circ}C$
  - This requires a lot of repetition due to temperature ramp from internal heating
- Use and correct the eff1 measurement calculated in <u>pbv3\_eff\_temp\_scan.cpp</u> (powertools)
  - Two efficiency values calculated
    - eff1 is dependent on VOUT, IOUT, VIIN, IIN, and IIN\_offset (Id, Id, ps, ps, ps)
    - eff2 is dependent on VDCDC, IOUT, DCDCIN, IIN, and IIN\_offset (amac, Id, amac, ps, ps)
      - Id measurements are from the DC variable load BK85xxx
      - ps measurements are from the power supply
      - amac measurements are from the ADCs on the AMAC chip

### Taking data well (cont.)

- When probing output voltage on the board at C10 with multimeter when DCDC set to 0A, voltage matches VOUT
  - C10 = 1.57V, VOUT = 1.57V, VDCDC = 1.35V
  - Conclusion: use eff1
- Modified eff1 to account for voltage drop across the long copper trace
  - At IOUT = 3.5A, C10 = 1.54V, VOUT = 1.26V
  - Graphed |VOUT C10| vs. IOUT to find trace resistance (slope) was  $0.0775\Omega$ 
    - » Accounted for the  $0.0775\Omega$  offset by using (VOUT + 0.0775\*IOUT) instead of VOUT



# Taking data well (cont.)

- Run calibrations in <u>pbv3\_tune.cpp</u> a singular time before data collection commences
  - <u>calibrateSlope</u>, <u>calibrateOffset</u>, <u>tuneVDDBG</u>, <u>tune AMBG</u>, <u>tuneRampGain</u>, <u>calibrateNTC</u>, <u>calibrateTemperature</u>
- Run <u>calibrateAMACslope</u> at the beginning of each data collection set (multiple collection sets in while loop)
  - Should saturate at 1023 counts around 0.9V input voltage
    - Prior to running tunings, AMAC slope wasn't saturating, reaching 850 counts at 1V
  - Usually takes three minutes to stabilise
  - Modified data collection approach to accommodate this
- Each measurement (multiple measurements per collection set) must stabilise at a given output current before the data is taken

#### Taking data well (cont.)

- Temperature increases non-uniformly with output current due to internal heating
  - Due to non-uniform heating, scanning current is hard for data collection
  - Scanning temperature for a fixed current value is possible, but takes a while
    - Chiller temperature must stabilise before data collection
  - Solution: Scan currents that satisfy specific temperature bins, and then grossly scan temperature

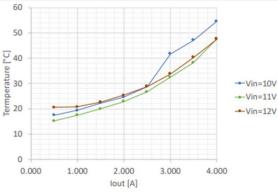
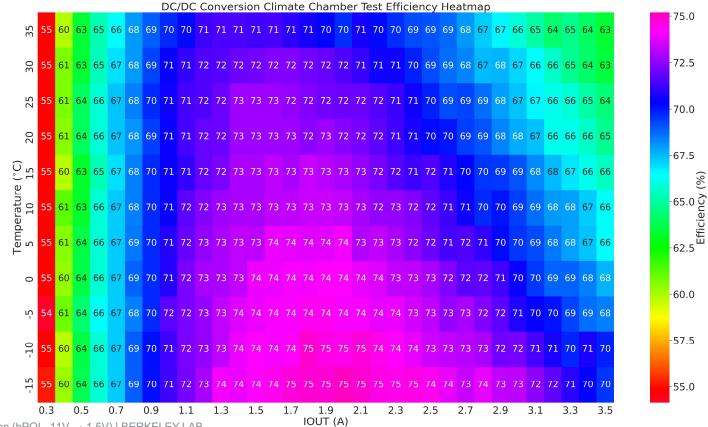


Figure 26: Increase of temperature for the Vout=1.5V version with Vin and Iout, with the module in good thermal contact with a cooling plate at about  $20^{\circ}$ C.

#### **Efficiency Heatmap**



10

DC/DC Conversion (bPOL,  $11V \rightarrow 1.5V$ ) | BERKELEY LAB

#### Fit equation

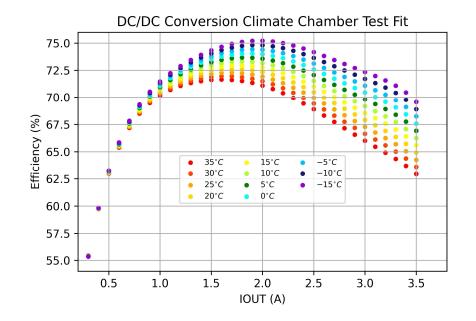
*P* is PTAT (°C), *I* is IOUT (A)

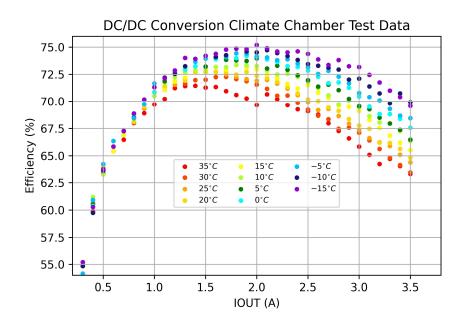
E(P, I)

 $= (0.00245273 \cdot P - 0.56929)I^{6} + (-0.0268157 \cdot P + 7.1382)I^{5} + (0.112837 \cdot P - 35.8580)I^{4} + (-0.224422 \cdot P + 92.854)I^{3} + (0.206925 \cdot P - 134.97)I^{2} + (-0.122281 \cdot P + 110.298)I + (0.0254751 \cdot P + 32.1888)$ 

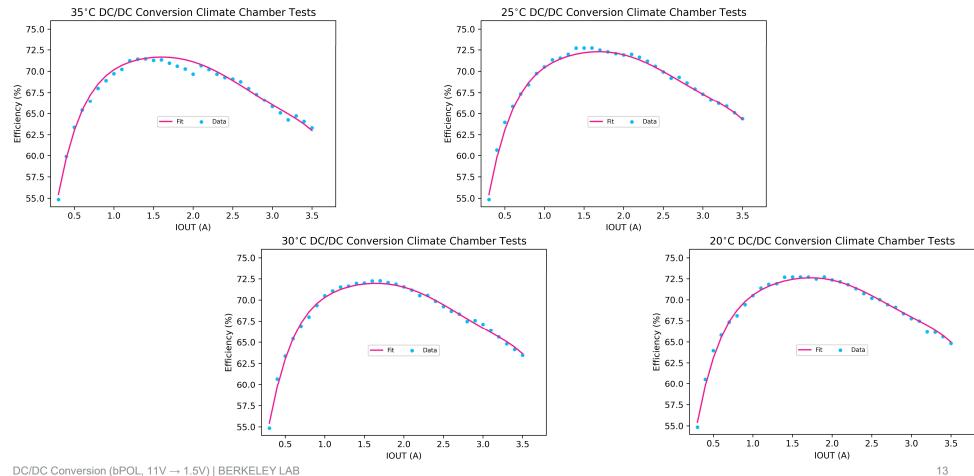
DC/DC Conversion (bPOL, 11V → 1.5V) | BERKELEY LAB

#### Fit vs. Data



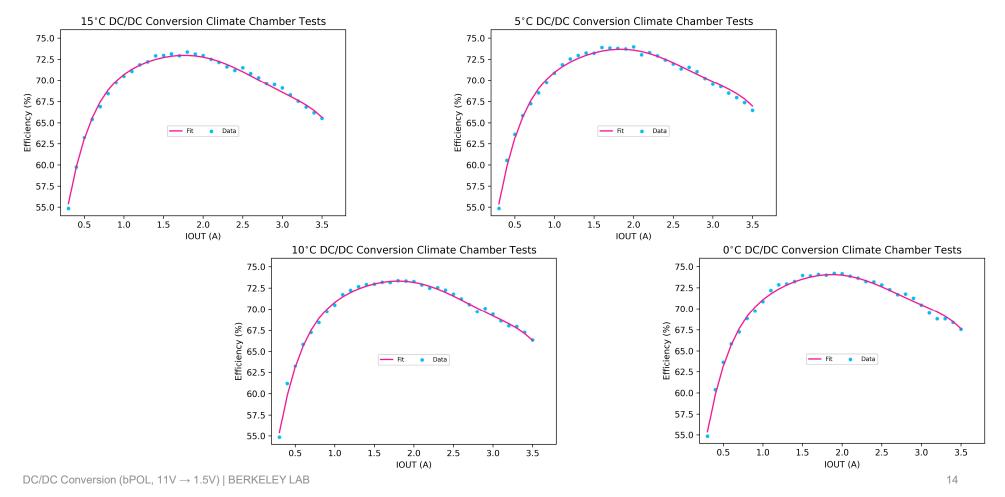


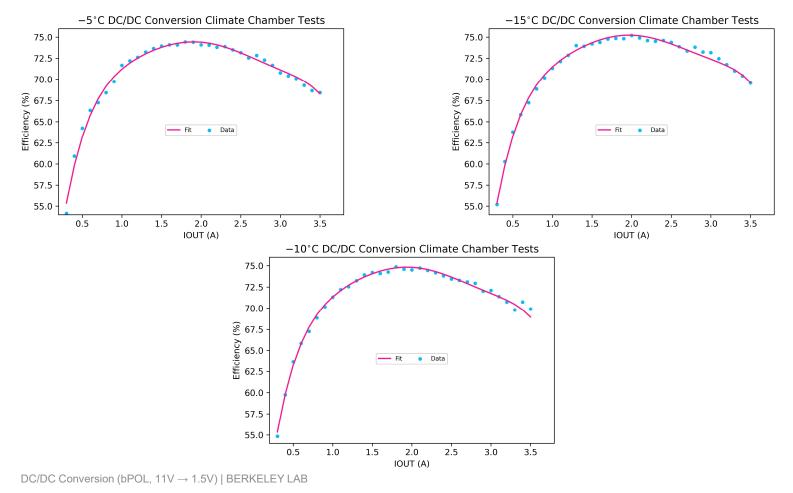
DC/DC Conversion (bPOL,  $11V \rightarrow 1.5V$ ) | BERKELEY LAB



#### Fit vs. Data (above room temp)







#### Fit vs. Data (below freezing)

# **Thank You!**

DC/DC Conversion (bPOL, 11V  $\rightarrow$  1.5V) | BERKELEY LAB